

# 10th U.S. National Combustion Meeting:

Validation and uncertainty quantification analysis (VUQ) of a  
char oxidation model

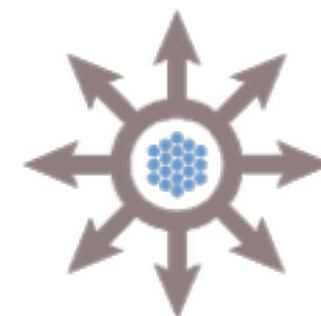
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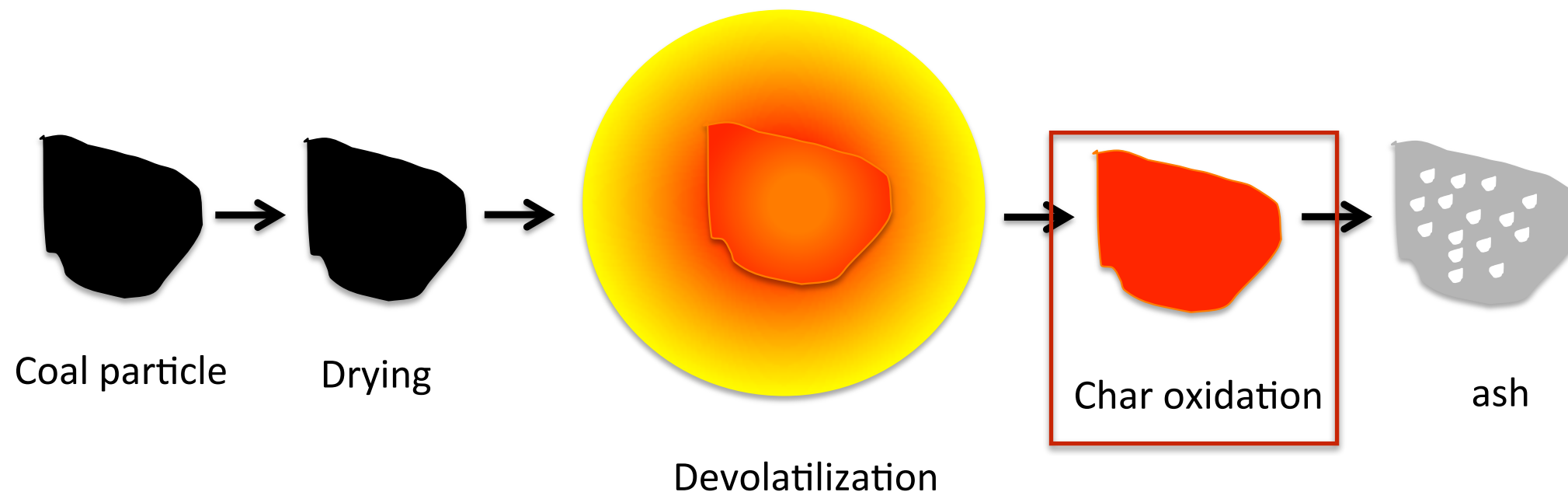
Sandia National Laboratories  
Livermore, California

April 23–26, 2017  
College Park, Maryland



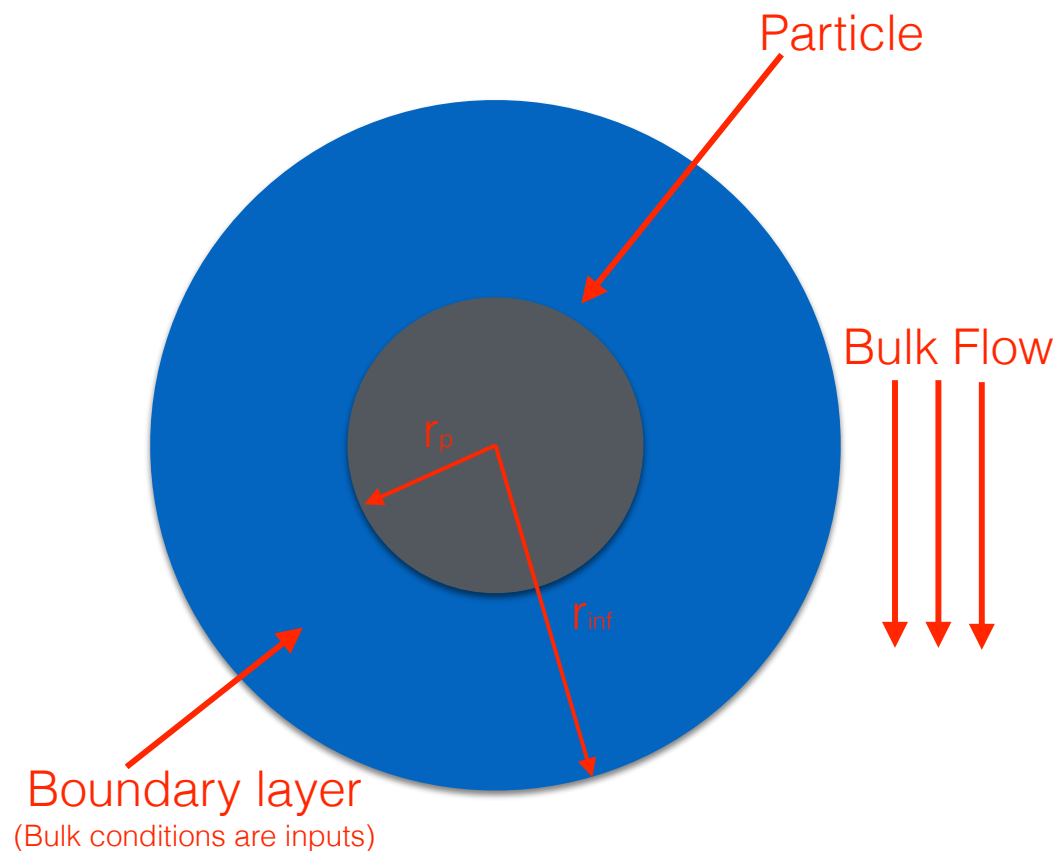
# Char oxidation

Char oxidation is the last stage of the coal combustion process. It is the slower stage of the process and can take place in the whole combustion space.



- Involved in calculations of temperature and gas composition.

# Reacting Particle and Boundary Layer (RPBL) model



- Computes transient-state conditions for a spherical, constant-diameter, reacting, porous char particle and its reacting boundary layer.
- Transport of gaseous species uses Maxwell-Stefan multicomponent approach.
- Homogeneous gas phase reactions are estimated with a syngas mechanism.
- Heterogeneous reactions are calculated with a six-step reaction mechanism.
- Computes carbon consumption, uses Bhatia and Perlmutter model to estimate surface area evolution.
- Solves one energy equation for the gas and one for the particle.
- Physical properties depend of the fractions of ash and carbon and on void fraction.

Reaction	$A[\text{mol}, \text{cm}^2, \text{s}]$	$E[\text{kJ/mol}]$
$C_b + C_s + O_2 \rightarrow CO + C(O)_s$	$3.3 \times 10^{15}$	167.4
$C(O)_s + C_b \rightarrow CO + C_s$	$1.0 \times 10^8$	0.0
$C_s + O_2 \rightarrow C(O_2)_s$	$9.5 \times 10^{13}$	142.3
$C(O_2)_s + C_b \rightarrow CO_2 + C_s$	$1.0 \times 10^8$	0.0
$C_s + CO_2 \rightarrow CO + C(O)_s$	variable	251.0
$C_s + H_2O \rightarrow H_2 + C(O)_s$	variable	222.0

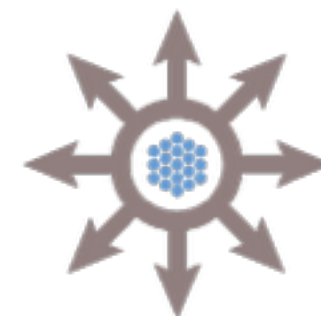
# RPBL model equations

## Energy equations

$$\frac{dT_{g,i}}{dt} = \frac{1}{\rho_{t,i} c_{p g,i} V_i} \left[ \underbrace{- [(AF_{cond})_{i+1/2} - (AF_{cond})_{i-1/2}]}_{\text{Conduction}} - \underbrace{[(AF_h)_{i+1/2} - (AF_h)_{i-1/2}]}_{\text{Enthalpy}} - V_i \rho_{t,i} \sum_{k=1}^{Kg} h_{k,i} \frac{dY_{k,i}}{dt} + \underbrace{S_i}_{\text{Heat exchange between solid and gas}} \right]$$

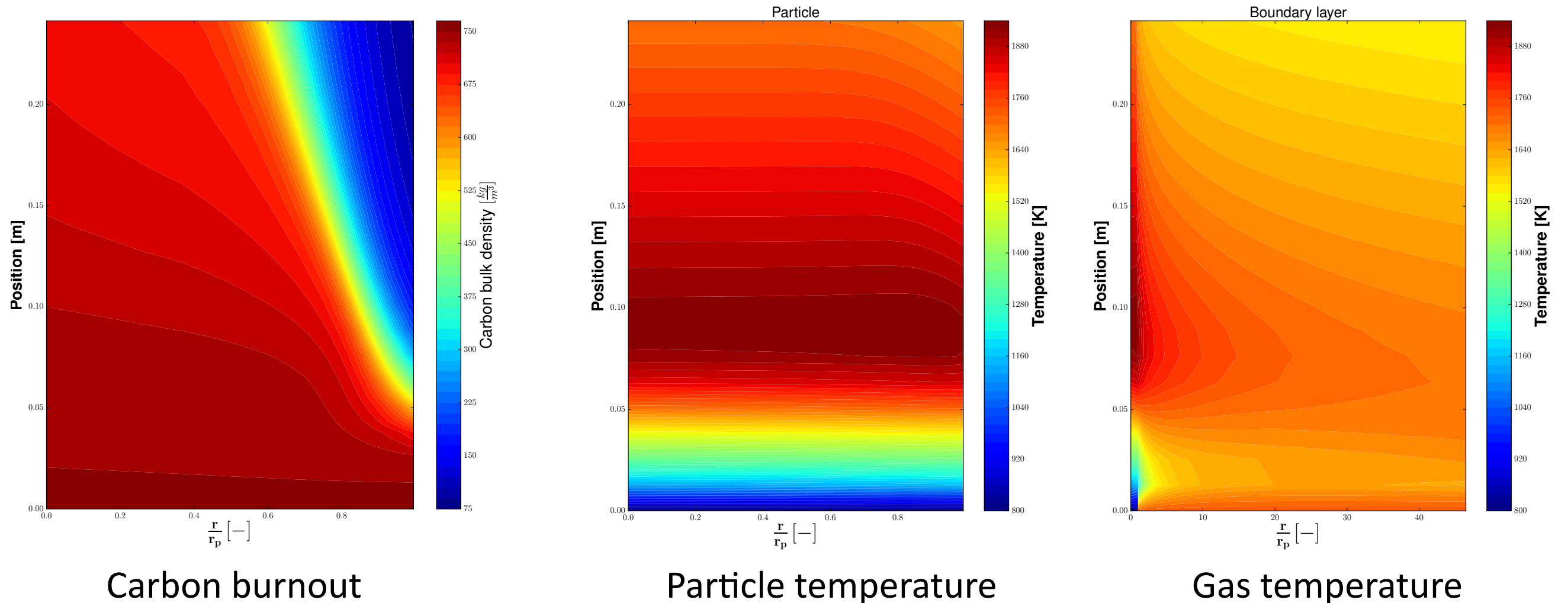
Transient term

$$\frac{dT_{p,i}}{dt} = \frac{1}{\rho_{bulk p,i} c_{p p,i} V_i} \left[ \underbrace{- [(AF_{cond,p})_{i+1/2} - (AF_{cond,p})_{i-1/2}]}_{\text{Conduction}} - \underbrace{h_{cb,i} \dot{s}_{cb,i} \sigma_{r,i} V_i}_{\text{Enthalpy}} - \underbrace{S_i}_{\text{Heat exchange between solid and gas}} \right]$$



# RPBL model results

## Base case



N= 60, N<sub>p</sub> = 30; RPBL solved 781 ODEs

$$\tau = 5, \frac{r_{inf}}{r_p} = 53, \psi = 8, \varepsilon_p = 0.96, \lambda_p = 1.33, d_p = 95 \mu m,$$

$$\phi_{initial} = 0.18, Y_{c,initial} = 0.98, Sgc_{initial} = 8000 [kg_c/m^2]$$

## Step 1: Selection of quantities of interest (QOIs)

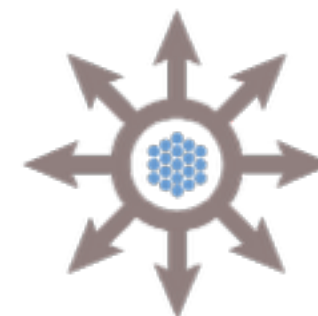
- Particle temperature and velocity (experimental data collected by Hecht).
- Three chars obtained from Illinois #6 (high volatile bituminous coal), Utah Skyline (western bituminous coal), and Black Thunder (subbituminous coal).
- Two environments:  $O_2$  = (24, 36 vol%),  $H_2O$  = (14 vol%, balance  $CO_2$ ).
- Average particle temperature from RPBL is used.

## Step 2: Input/Uncertainty Map

Parameter	Priority	Range		Nominal value
		min	max	
Numerical Parameters				
$N_p$	1	15	100	30
$N$	1	30	200	60
$rtol$	1			1e-4
Model Parameters				
$\tau [-]$	6	3	6	
$\frac{r_{inf}}{r_p} [-]$	6	50	120	
$\psi [-]$	6	3	8	
$\epsilon_p [-]$	6	0.1	1	
$\lambda_p [\frac{W}{mK}]$	6	0.1	2	
$\rho_{true c} [\frac{kg}{m^3}]$	1			921
$\rho_{true ash} [\frac{kg}{m^3}]$	1			2000
$h_{solid gas} [\frac{W}{m^2K}]$	1			1
Scenario parameters				
$d_p [\mu m]$	6	50	160	
$v_g [\frac{m}{s}]$	3			From reactor model
$T_g [K]$	3			From reactor model
$O_{2,bulk} [-]$	3			From reactor model
$H_{2O,bulk} [-]$	3			From reactor model
$CO_{2,bulk} [-]$	3			From reactor model
$H_{2,bulk} [-]$	3			From reactor model
$CO_{bulk} [-]$	3			From reactor model
$O_{2,initial} [-]$	3			1.00e-3
$H_{2O,initial} [-]$	3			1.00e-3
$H_{2,initial} [-]$	3			1.00e-3
$CO_{initial} [-]$	3			1.00e-3
$CO_{2,initial} [-]$	3			0.99
$T_{p,initial} [K]$	3			From reactor model
$\phi_{initial}$	6	0.15	0.7	
$Y_{c,initial} [-]$	6	0.5	1	
$Sgc_{initial} [\frac{kg}{m^2}]$	6	8000	12000	
$T_w [K]$	3			500
$Pressure [\frac{kg}{m^2}]$	3			1.00e5

- Sensitivity analysis with eight active parameters for three particle sizes (50  $\mu m$ , 80  $\mu m$ , 120  $\mu m$ )
- Particle size is the ninth parameter
- Test sensitivity of particle temperature and velocity.

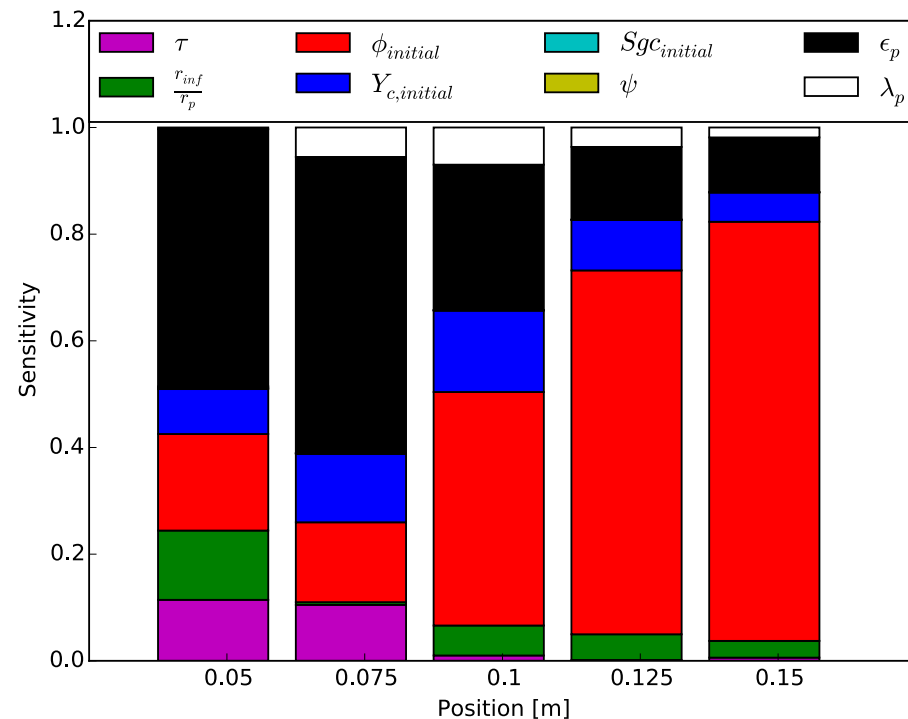
- Small-size particles      53 – 60  $\mu m$
- Medium-size particles      75 – 90  $\mu m$
- Big-size particles      106 – 125  $\mu m$



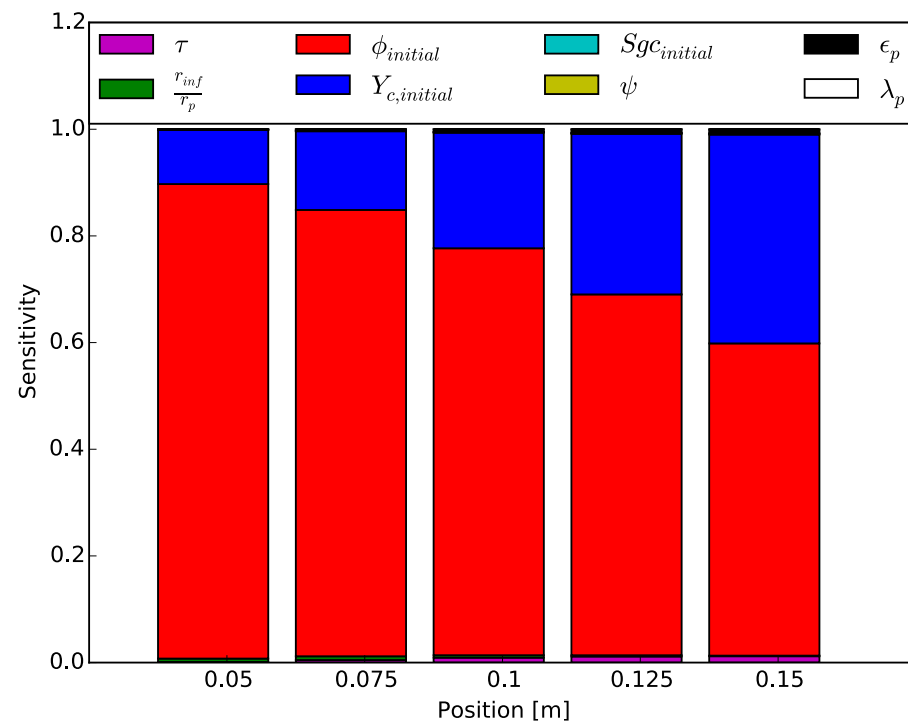
CARBON CAPTURE  
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## Step 2: Input/Uncertainty Map



Particle temperature



Particle velocity

### General

- 256 RPBL cases were run.
- Uncertainty Quantification Toolkit (UQTK)
- Use coefficients of first order polynomial chaos surrogate model.

$$d_p = 80 \mu m \text{ (} 75 - 90 \mu m \text{)}$$

### Particle temperature

- Most sensitive parameters were  $\phi_{initial}$ ,  $Y_c$ , and  $\epsilon_p$
- Next were  $\frac{r_{inf}}{r_p}$ ,  $\tau$  and  $\lambda_p$
- Least sensitive parameters were  $Sgc_{initial}$  and  $\psi$

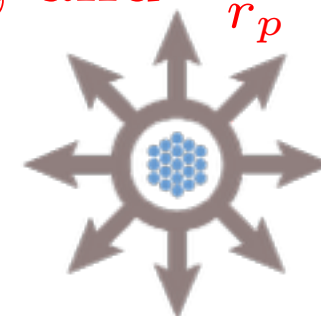
### Particle velocity

- Most sensitive parameters were  $\phi_{initial}$ , and  $Y_c$

### Conclusion

- Five parameters were selected for consistency analysis:

$$d_p, \phi_{initial}, Y_c, \epsilon_p, \text{ and } \frac{r_{inf}}{r_p}$$

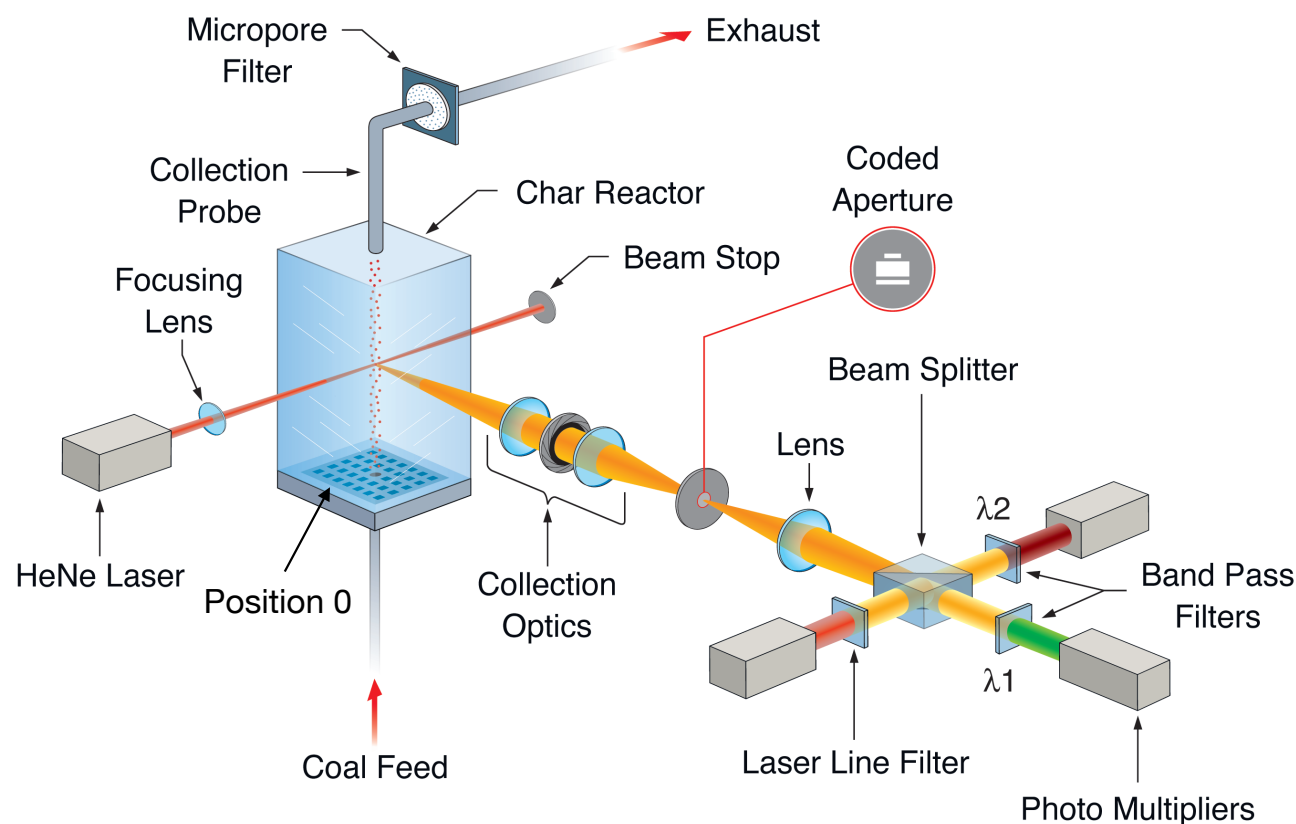


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## Step 3: Experimental data collection

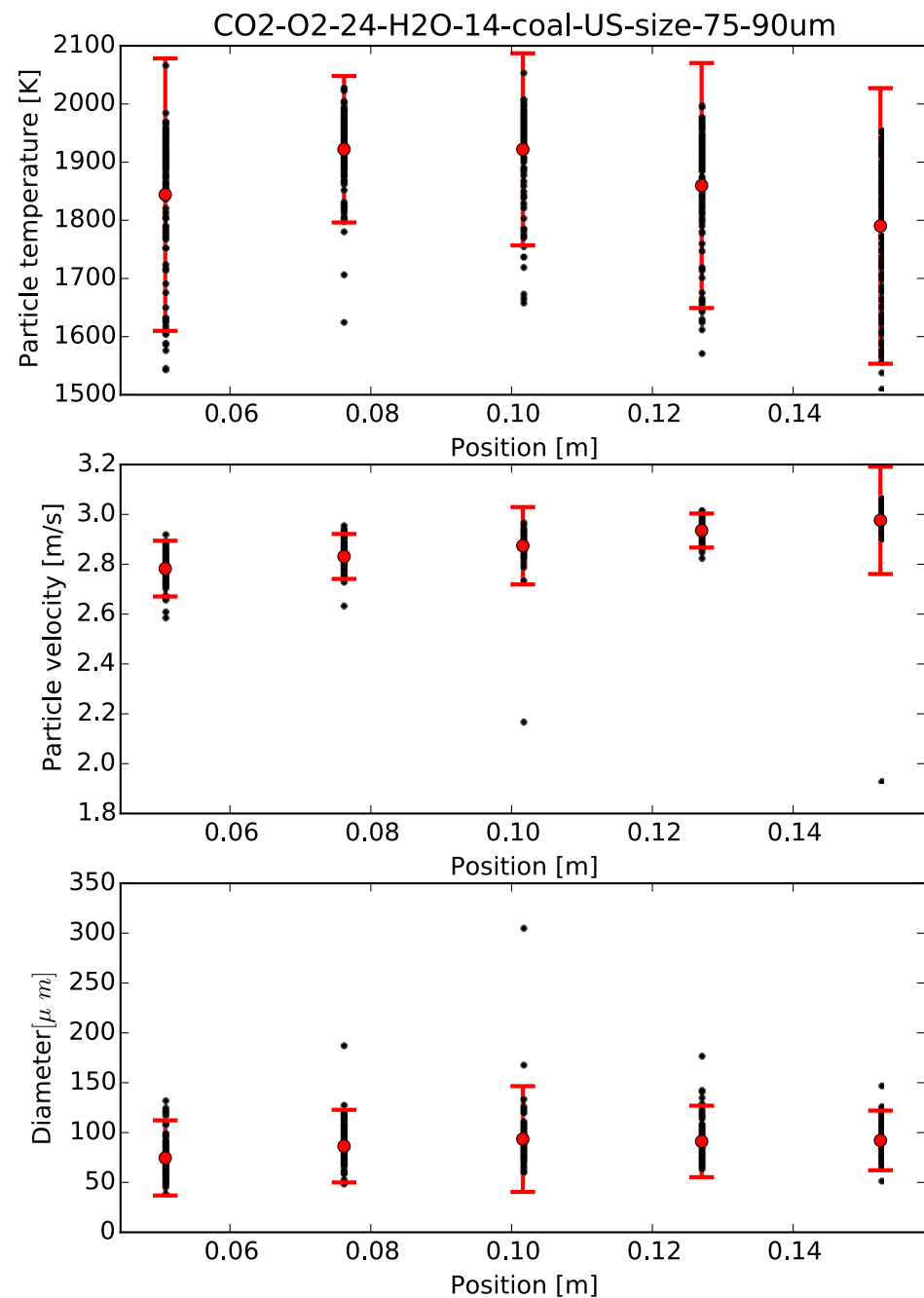
Laminar, entrained flow reactor at Sandia National Laboratories.



- Three types of measurements: temperature, velocity and size of a single particle.
- Three type of char : Illinois #6 (I6), Utah Skyline (US), Black Thunder (BT).
- Two environment conditions:  
 $O_2 \text{ vol\%} = 24, 36; H_2O \text{ vol\%} = 14$  balance  $CO_2$
- Six bin sizes :  
 $53\text{-}63 \mu m, 63\text{-}75 \mu m, 75\text{-}90 \mu m,$   
 $90\text{-}106 \mu m, 106\text{-}125 \mu m,$  and  $125\text{-}150 \mu m$
- In each position approximately 100 particles are measured.

# Step 3: Experimental data collection

## Uncertainties in experimental measurements



Systematic error

$$\bar{y} - y_T = \Delta + \beta$$

Sampling error

$$|\beta| \leq t_{\alpha/2, v} \frac{s}{\sqrt{n}}$$

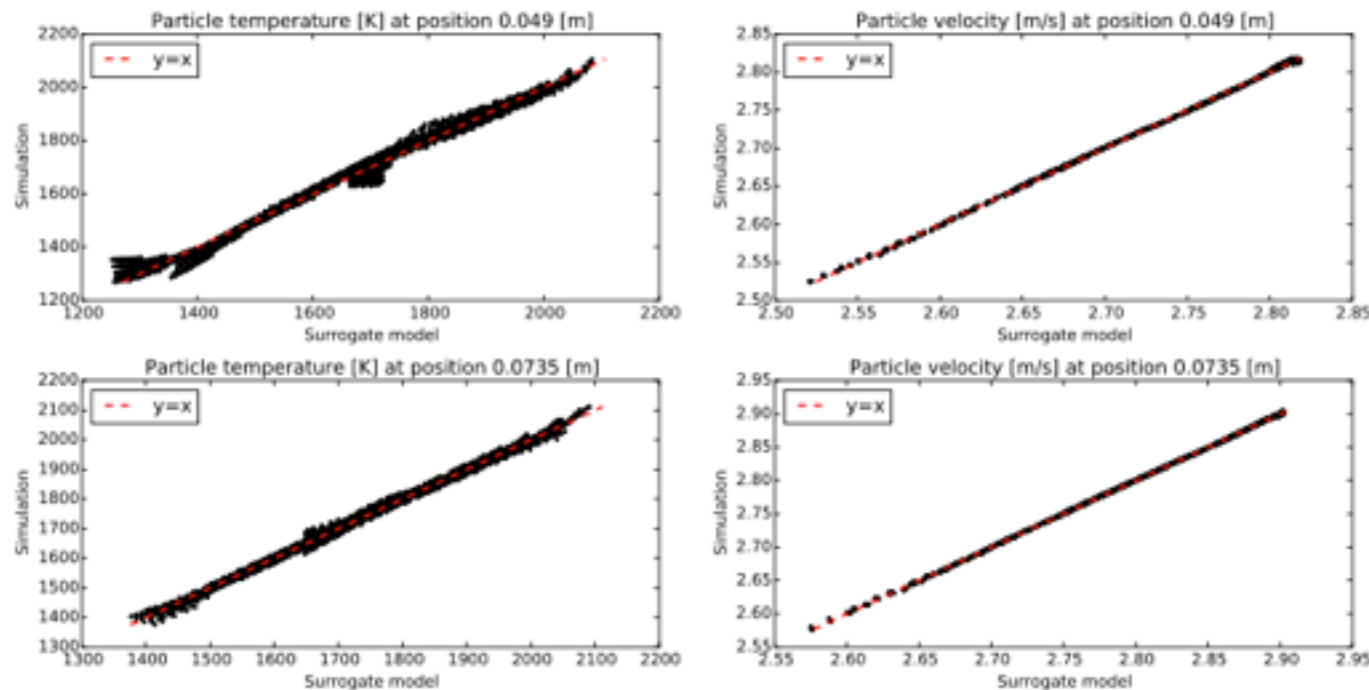
- Systematic error is assumed much smaller than random error.
- Experiment is defined as one char, one environment, and one particle size at all measurement positions in the reactor.
- Sampling error was computed for 36 experiments using a confidence interval of 95 %.

## Step 3: Simulation data collection

### RPBL model

- RPBL was run using average temperature and velocity profiles from reactor model
- Five parameters were used:  $d_p$ ,  $\phi_{initial}$ ,  $Y_c$ ,  $\epsilon_p$ , and  $\frac{r_{inf}}{r_p}$
- Uncertainty Quantification Toolkit (UQTk) was used to produce a design of experiments.
- 10901 cases were run.
- Each case has 60 cells, therefore RPBL is solving 781 ODEs.
- RPBL cases were run on linux cluster at the University of Utah; with 520 cores it was possible to run all cases in one day.

## Step 4: Construction of surrogate models

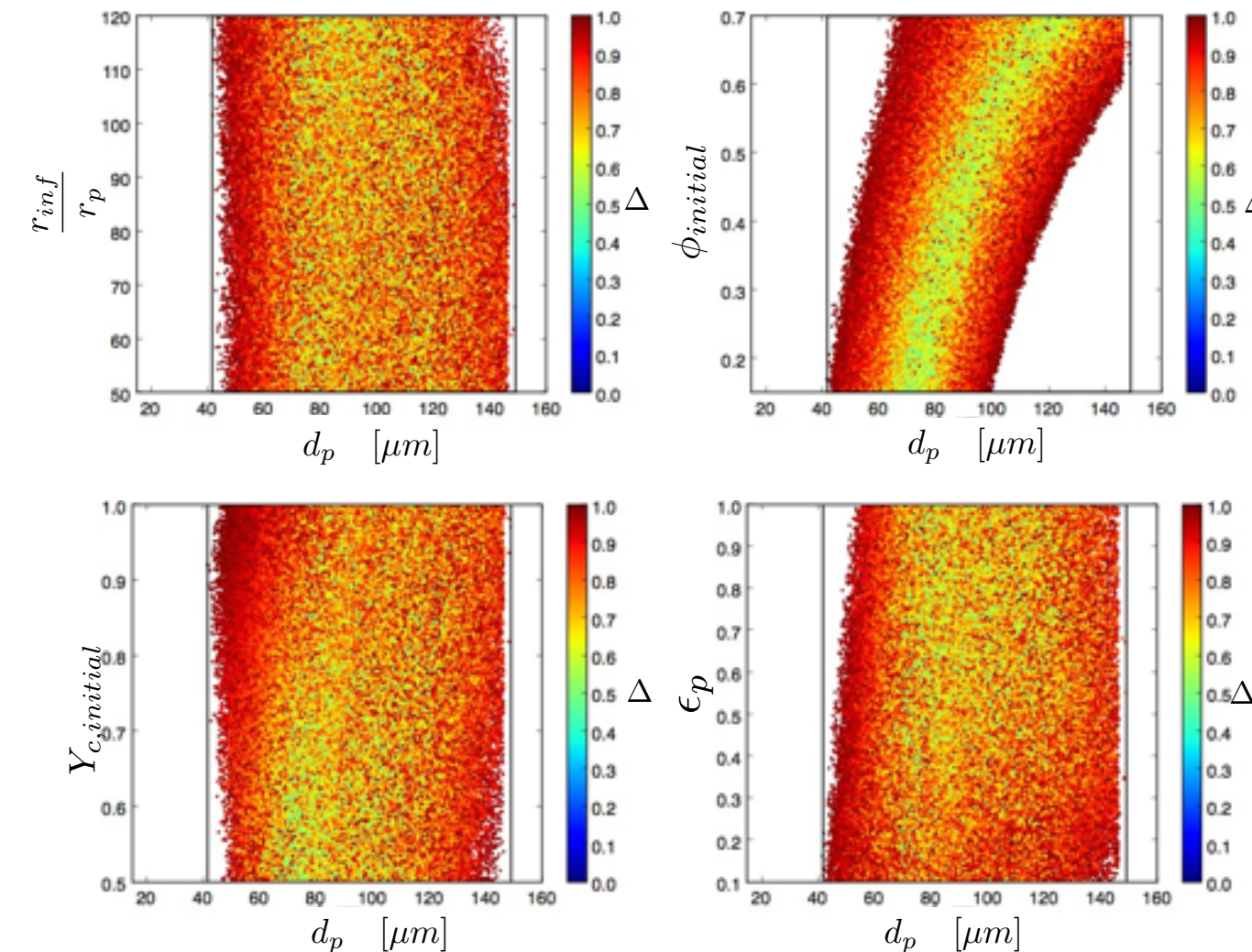


- Surrogate models for particle temperature and velocity are created for each measurement location.

- PC of order 4 was used for  $O_2 = 24 \text{ vol } \%$ ,  $H_2O = 14 \text{ vol } \%$ , balance  $CO_2$  environment; 3125 cases were run.
- PC of order 5 was used for  $O_2 = 36 \text{ vol } \%$ ,  $H_2O = 14 \text{ vol } \%$ , balance  $CO_2$  environment; 7776 cases were run.

## Step 5: Analysis of model outputs

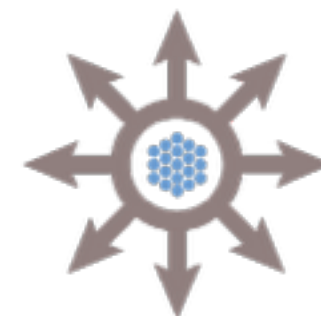
US char  $O_2 = 24 \text{ vol\%}$ ,  $H_2O = 14 \text{ vol\%}$ , balance  $CO_2$  environment 75-90  $\mu\text{m}$  size bin



- Consistency analysis was carried out for 36 experiments performed by Hecht.
- Experimental particle size was used as prior range.
- Same set of RPBL data is used for the three chars.

$$\frac{|y_{m,e}(\mathbf{x}) - y_e|}{u_e} \leq 1$$

Parameter	Prior range	Consistent range	Nominal value
$d_p$ [ $\mu\text{m}$ ]	36.9- 146.5	42.0-146.0	75-90
$\phi_{initial}$	0.15 - 0.7	0.15 - 0.7	-
$Y_{c,initial}$ [-]	0.5-1	0.5-1	-
$\frac{r_{inf}}{r_p}$ [-]	50-120	50-120	-
$\epsilon_p$ [-]	0.1-1	0.1-1	-

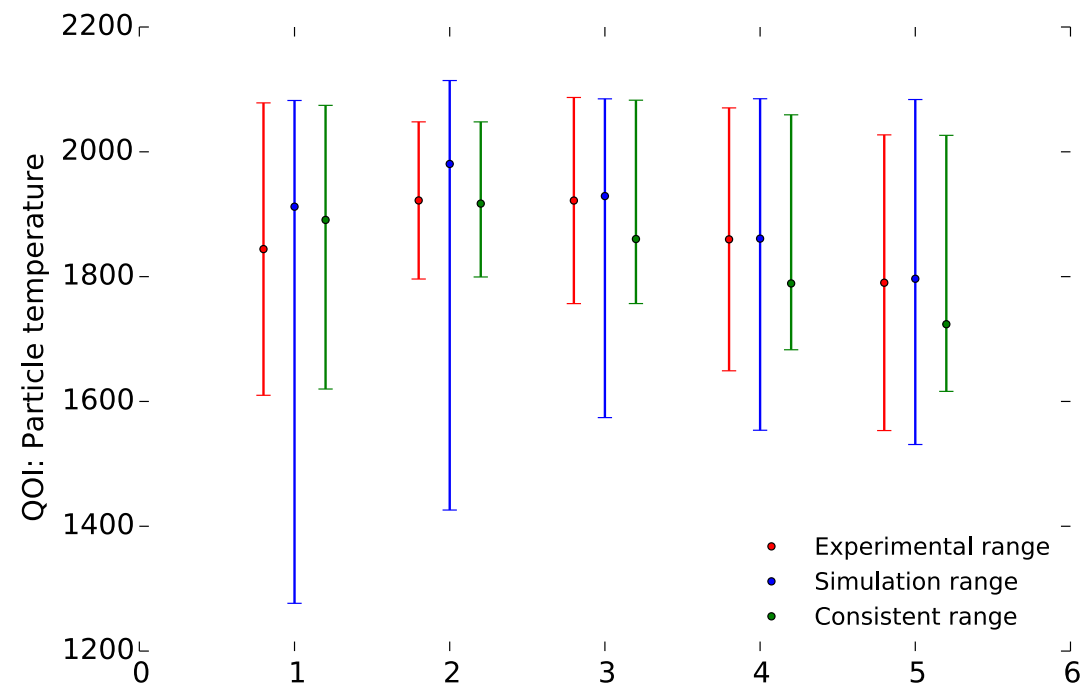


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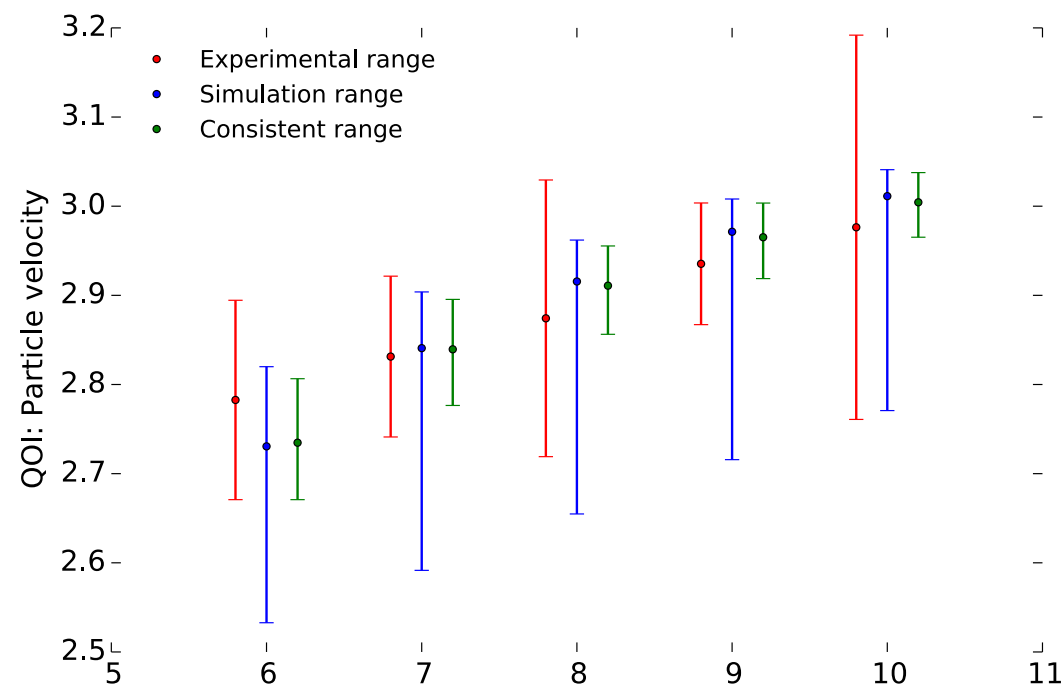


## Step 5: Analysis of model outputs

US char  $O_2 = 24 \text{ vol\%}$ ,  $H_2O = 14 \text{ vol\%}$ , balance  $CO_2$  environment 75-90  $\mu m$  size bin



We performed a similar consistency analysis for the other 35 experiments and obtained consistency with all 36 experiments.



## Step 6: Feedback and feed forward Model

- Transient RPBL model for char oxidation was developed. Assumptions in the formulation include:
  - Diameter of the particle during the combustion process was constant.
  - Gradient of pressure was assumed negligible.
  - Same heterogeneous reaction mechanism was used for all three chars.
- QOIs (particle temperature and velocity) are most sensitive to  $d_p$ ,  $\phi_{initial}$ ,  $Y_c$ ,  $\epsilon_p$ 
  - Consistency was found for 36 experiments if experimental size of particle is used as prior range.
  - Develop models of coal devolatilization that predict void fraction and carbon mass fraction.
  - Use a better classification system for characterizing the size distribution of particles.
- Increase the number of measurements at each position in order to reduce the sampling error.



# Acknowledgment

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